

# $e^+$ Collection systems

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- The QWT consist of two magnetic field region.
- The first solenoid has a strong magnetic field  $B_1$  over a length  $L_1$
- The second solenoid has a weaker magnetic field  $B_2$  over a length  $L_2$
- The phase space acceptance for a QWT is calculated from the global transfer matrix:

$$\begin{pmatrix} X \\ P_X \end{pmatrix} = \begin{pmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{pmatrix} \begin{pmatrix} X_0 \\ P_{X_0} \end{pmatrix}$$

- From the previous matrix we can get the phase space transport over a QWT:

$$\begin{aligned}
 XX^* + \left(\frac{2}{eB_2}\right)^2 P_X P_X^* &= \left[ \cos^2 \chi_1 + \left(\frac{B_1}{B_2}\right)^2 \sin^2 \chi_1 \right] x_0 x_0^* & (1) \\
 &+ \left[ \left(\frac{2}{eB_1}\right)^2 \sin^2 \chi_1 + \left(\frac{2}{eB_2}\right)^2 \cos^2 \chi_1 \right] p_{x_0} p_{x_0}^* \\
 &+ \frac{2}{eB_1} \sin \chi_1 \cos \chi_1 \left[ 1 - \left(\frac{B_1}{B_2}\right)^2 \right] (x_0^* p_{x_0} + x_0 p_{x_0}^*)
 \end{aligned}$$

- Where  $X^* \equiv x + iy$  and  $P_X^* \equiv p_x + ip_y$  and.

- Using  $\chi_1 = \pi/2$ , the previous formula is reduced to :

$$\left(\frac{eB_2}{2}\right)^2 XX^* + P_X P_X^* = \left(\frac{eB_2}{2}\right)^2 (x^2 + y^2) + (p_x^2 + p_y^2) = \text{Cte}$$

- Which can be expressed in a cylindrical coordinate system as:

$$\left[\frac{B_1}{B_2}\right]^2 r_0^2 + \left[\frac{2}{eB_1}\right]^2 \left[ P_{r_0}^2 + \frac{P_{\phi_0}}{r^2} \right] = \text{Cte}$$

- The positron emitted at the converter with phase space coordinates  $(X_0, P_{X_0})$  are transmitted only if :

$$XX^* \leq a^2$$

- Thus we can write:

$$\text{Cte} - \left(\frac{2}{eB_2}\right)^2 P_X P_X^* \leq a^2$$

- At  $P_{r_0} = P_{\phi_0} = 0$  we can define the QWT radial acceptance:

$$r_0^{max} = \frac{B_2}{B_1} a$$

- Similarly, the radial momentum acceptance is defined by:

$$p_{r_0}^{max} = \frac{eB_1 a}{2}$$

- At a given momentum, The QWT volume acceptance is maximized:

$$\frac{dV(\chi_1)}{d\chi_1} = 0$$

- Which leads to:

$$p_m = \frac{eB_1 L_1}{n\pi}$$

- For  $B_1 = 2.5 T$  and  $B_2 = 0.5 T$  and  $p_m = 60 \text{ MeV}/c$ , the optimal length is set at  $L_1 = 25 \text{ cm}$ .
- The radial acceptance for an aperture radius  $a = 3 \text{ cm}$  :

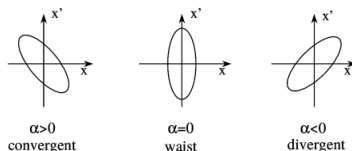
$$r_0^{max} = \frac{B_2}{B_1} a = 1.5 \text{ cm}.$$

- The radial momentum acceptance is set at :

$$\theta_{r_0}^{max} = \frac{eB_1 a}{2p_m} = 0.18 \text{ [rad]} \quad (2)$$



- What about  $L_2$  ?
- Our goal is to decrease the initial transverse momentum meaning we want to rotate the  $(x-x')$  phase space using  $\pi/2$  rotation.



- The solenoid transfer matrix is defined as :

$$\begin{pmatrix} \cos^2(k l) & \frac{\sin(k l) \cos(k l)}{k} & \sin(k l) \cos(k l) & \frac{\sin^2(k l)}{k} \\ -k \sin(k l) \cos(k l) & \cos^2(k l) & -k \sin^2(k l) & \sin(k l) \cos(k l) \\ \sin(k l) (-\cos(k l)) & -\frac{\sin^2(k l)}{k} & \cos^2(k l) & \frac{\sin(k l) \cos(k l)}{k} \\ k \sin^2(k l) & \sin(k l) (-\cos(k l)) & -k \sin(k l) \cos(k l) & \cos^2(k l) \end{pmatrix}$$

- Where  $k = \frac{B}{2B\rho}$

- Using the twiss matrix transformation : 
$$\begin{bmatrix} \beta_{exit} \\ \alpha_{exit} \\ \gamma_{exit} \end{bmatrix} = M_{Twiss} \begin{bmatrix} \beta_0 \\ \alpha_0 \\ \gamma_0 \end{bmatrix}$$

- From the Solenoid matrix, the Twiss transport matrix is calculated:

$$\begin{bmatrix} \beta_{exit} \\ \alpha_{exit} \\ \gamma_{exit} \end{bmatrix} = \begin{pmatrix} -\frac{4 a_0 B R_0 \sin\left(\frac{B l}{2 B R_0}\right) \cos^3\left(\frac{B l}{2 B R_0}\right)}{B} + \frac{4 B R_0^2 G_0 \sin^2\left(\frac{B l}{2 B R_0}\right) \cos^2\left(\frac{B l}{2 B R_0}\right)}{B^2} + b_0 \cos^4\left(\frac{B l}{2 B R_0}\right) \\ a_0 \left( \cos^4\left(\frac{B l}{2 B R_0}\right) - \sin^2\left(\frac{B l}{2 B R_0}\right) \cos^2\left(\frac{B l}{2 B R_0}\right) \right) + \frac{B b_0 \sin\left(\frac{B l}{2 B R_0}\right) \cos^3\left(\frac{B l}{2 B R_0}\right)}{2 B R_0} - \frac{2 B R_0 G_0 \sin\left(\frac{B l}{2 B R_0}\right) \cos^3\left(\frac{B l}{2 B R_0}\right)}{B} \\ \frac{a_0 B \sin\left(\frac{B l}{2 B R_0}\right) \cos^3\left(\frac{B l}{2 B R_0}\right)}{B R_0} + \frac{B^2 b_0 \sin^2\left(\frac{B l}{2 B R_0}\right) \cos^2\left(\frac{B l}{2 B R_0}\right)}{4 B R_0^2} + G_0 \cos^4\left(\frac{B l}{2 B R_0}\right) \end{pmatrix}$$

- Where  $L_2 = l$  is the length of the second solenoid.
- $a_0$ ,  $b_0$  and  $G_0$  are the initial Twiss parameters calculated at the exit of the 1<sup>st</sup> solenoid.
- To get  $\pi/2$  rotation, we want to get  $\alpha_{exit} = 0$  and  $\beta_{exit} = \text{Max}$
- From the  $\beta_{exit}$  formula, we get the maximum value at  $l = 8.7$  m

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# Simulation : QWT initial parameters

- For the Polarized mode we have set the central momentum at 60MeV/c.
- The QWT parameters are
  - $B_1 = 2.5$  T
  - $L_1 = 0.25$  m
  - $B_2 = 0.5$  T
  - $l = L_2 = 8.7$  m
  - $r_0^{max} = 0.0015$  m
  - $\theta_0^{max} = 0.18$
- Only  $e^+$  contained inside the accepted ellipse will be transmitted at the exit of the QWT.

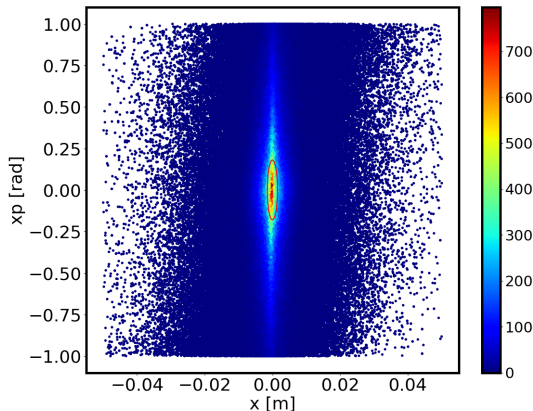
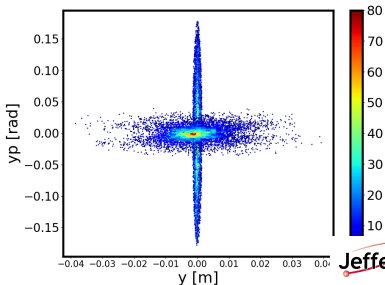
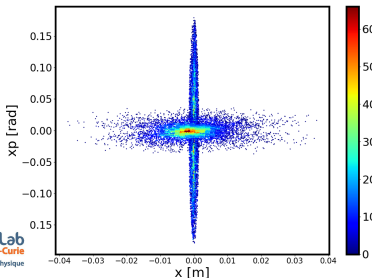
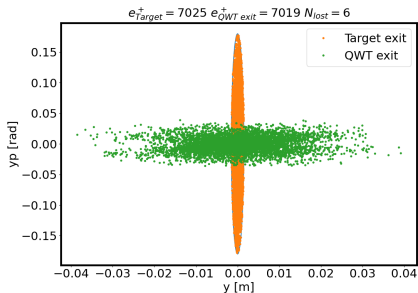
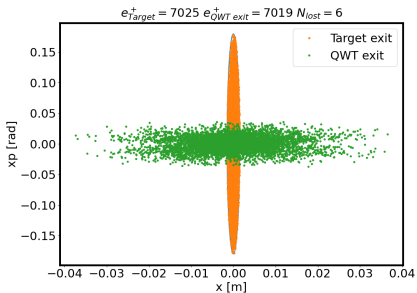
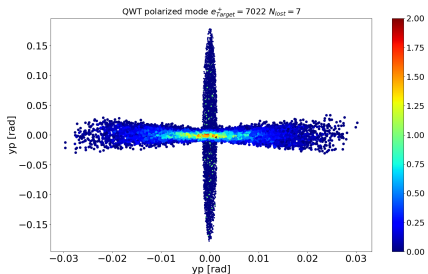
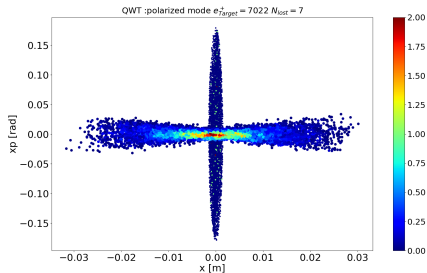


Figure:  $e^+$  At the Target

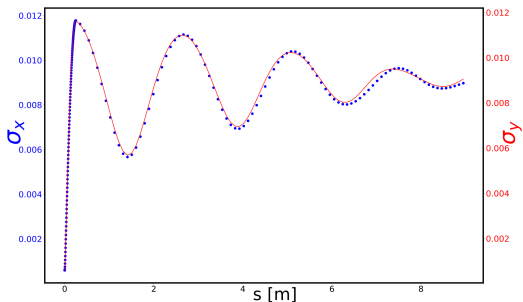
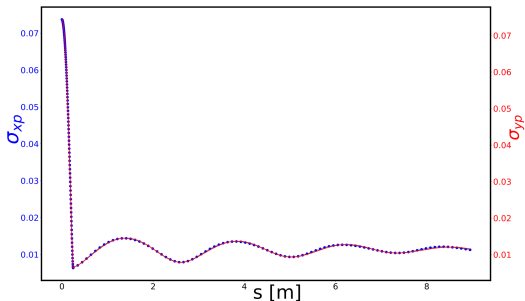
# QWT : Transverse phase space rotation



# QWT: Transverse phase space rotation $L_2 = 2.45\text{ m}$

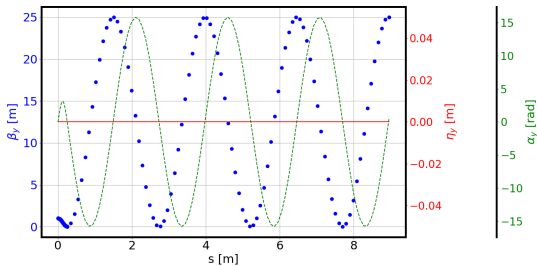
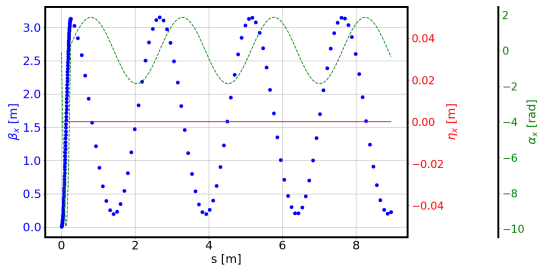


# QWT : Sigmas evolution

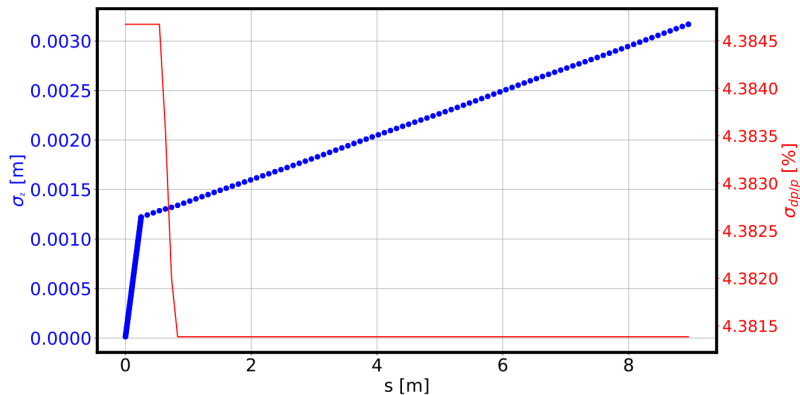




# QWT : Twiss functions



# QWT : Longitudinal plane



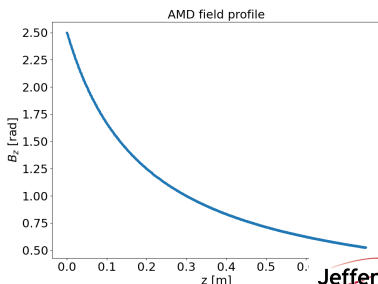
# AMD : initial parameters

- Using the same formulas, we can define the acceptance space phase parameters for the AMD:

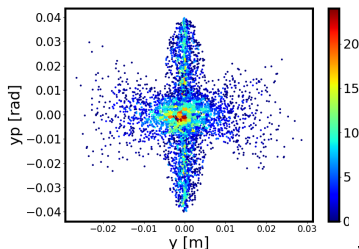
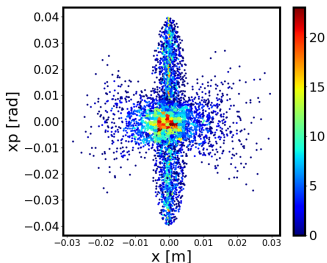
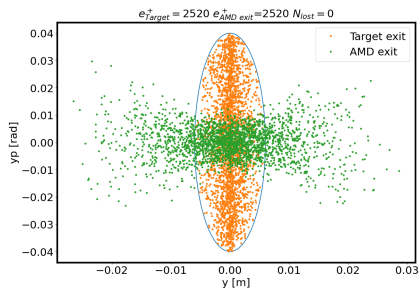
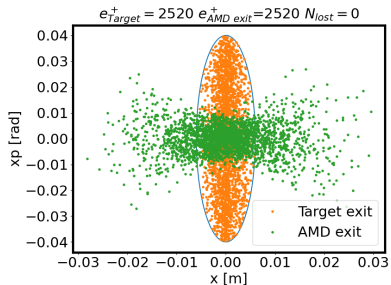
- The radial acceptance :  $r_0^{max} = \sqrt{\frac{B_2}{B_1}} a = 0.003 \text{ m}$ .
- To get the transverse momentum acceptance, we let  $x_0$  and  $p_{y0} = 0$ , then we get:

$$p_{x0}^{max} = \frac{1}{2} ea \sqrt{B_2 B_1} = 0.04 \text{ [rad]}$$

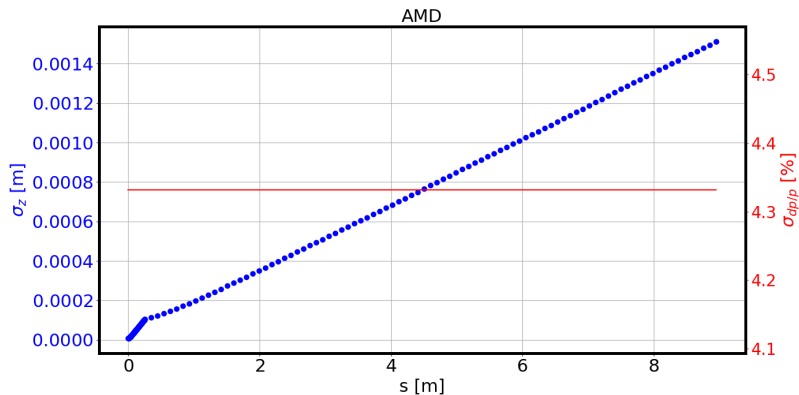
- To get a fair comparison, I will be using the same momentum cut used previously for the QWT case.
- AMD length  $L_{AMD} = 0.9 \text{ m}$
- $B_0 = 2.5 \text{ T}$
- $B_2 = 0.5 \text{ T}$



# AMD : Transverse phase space rotation



# AMD : Longitudinal plane



- The bunch length increase significantly in both cases : QWT and

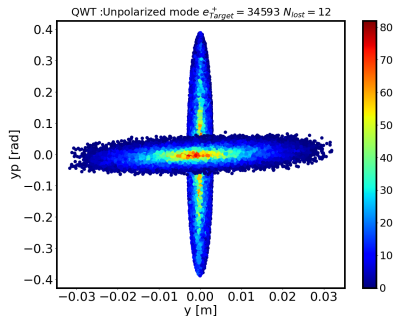
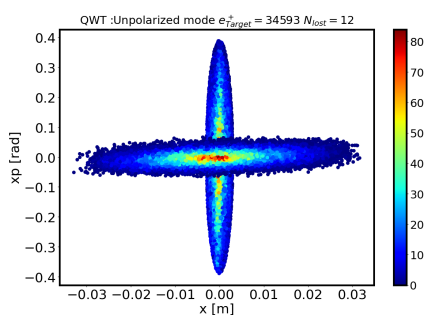
MD

- We shift the central momentum to 20 MeV/c, therefore the acceptances parametres will change too:

$$p_m = \frac{eB_1 L_1}{n\pi}$$

- leading to  $L_1 = 11 \text{ cm}$ ,  $B_1 = 1.8 \text{ T}$ ,  $B_2 = 0.2 \text{ T}$
- The radial acceptance for the unpolarized mode :  $r_0^{max} = 0.003 \text{ m}$
- The angular acceptance :  $\theta_0^{max} = 0.39 \text{ [rad]}$

# QWT : Transverse phase space rotation



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# QWT VS AMD

Parameters	QWT	AMD
Radial acceptance $r_0^{max}$ [m]	0.0015	0.003
Angular acceptance [rad]	0.18	0.04
$p_{e^+}$ MeV/c	[57-63]	[57-63]
1 <sup>st</sup> solenoidLength [m]	0.25	0.75
2 <sup>nd</sup> solenoidlength [m]	8.7	8.4
Number of $e^+$	7025	7025
Yield $e^+/e^-$	0.001405	0.001405
Transmission %	99.91	100
Longitudinal $\sigma_t$ [s]	$1.06 \cdot 10^{-11}$	$4.66 \cdot 10^{-12}$

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# Conclusion

- The radial acceptance is larger for the adiabatic device
- The angular acceptance is larger for the QWT
- The momentum acceptance is much larger for the adiabatic device. As a consequence, the accepted yield is higher
- The AMD is widely used with respect to high positron yield.
- The QWT may be interesting, if the yield is sufficient, to get a very clean beam, and to restrict the central momentum for easier transport.