

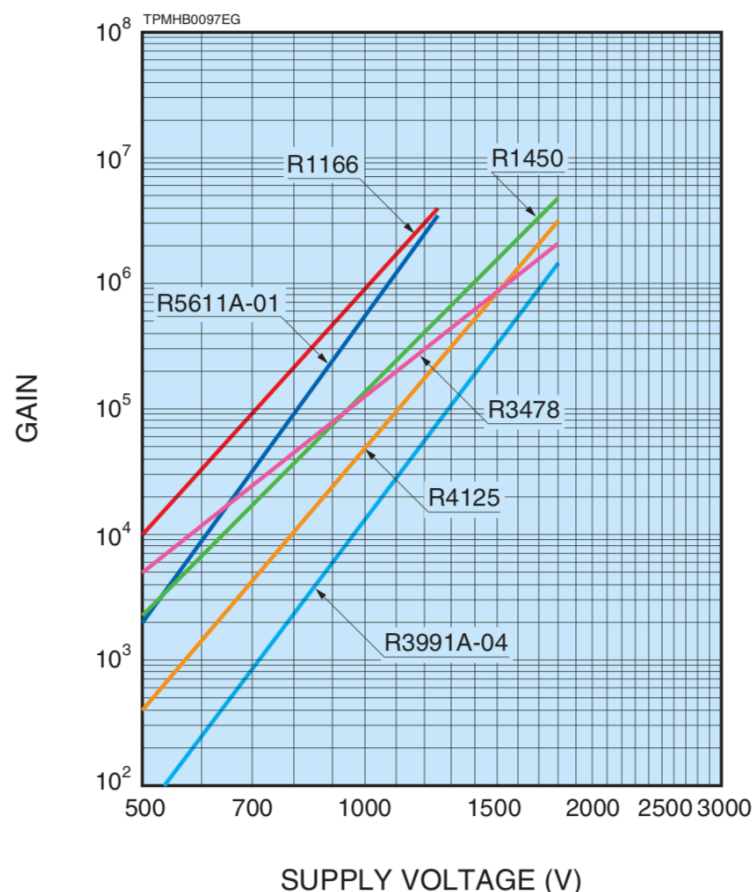
Comments related to some ERR slides

Rolf Ent and Bogdan W

June 6, 2019 meeting

R4125 gain and anode current

● 19 mm (3/4") Dia. types



Energy flow 1 rad/s ?? use 0.1 rad/s /per **1 uA**

0.1 rad/s $\Rightarrow 10^{-6}$ J/s/g $\Rightarrow 10^{-4}$ J/crystal
 $\Rightarrow 10^{15}$ eV/s $\Rightarrow 10^6$ GeV/s

signal has 15 ph.e./MeV for NPS scintillator

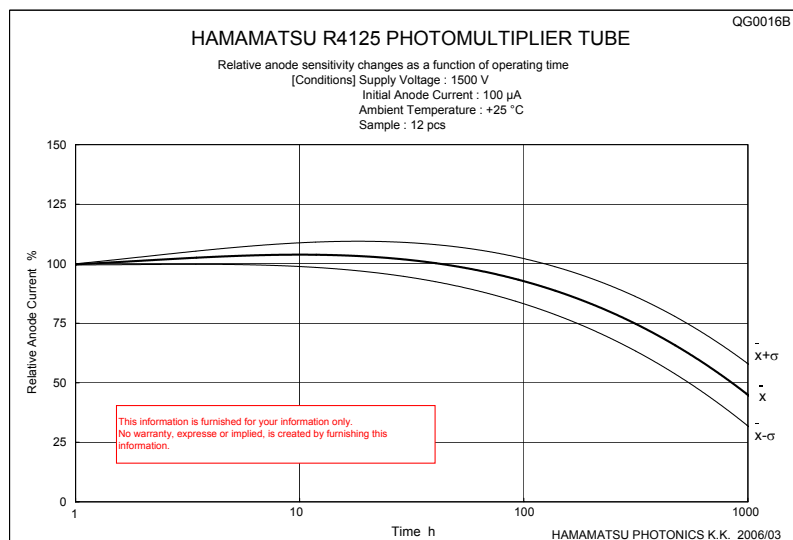
$\Rightarrow 1.5 \cdot 10^{10}$ ph.e./s in PMT gain of 10^5

\Rightarrow average anode current = **250 uA**

It is 2 times exceed the specs of R4125

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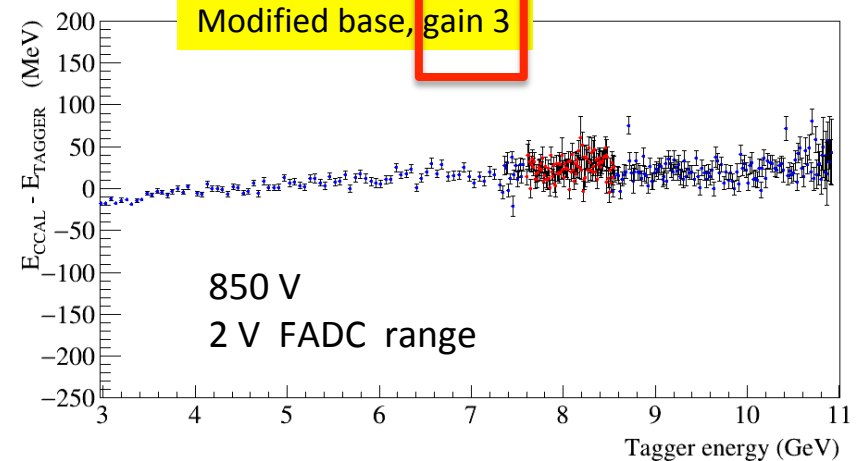
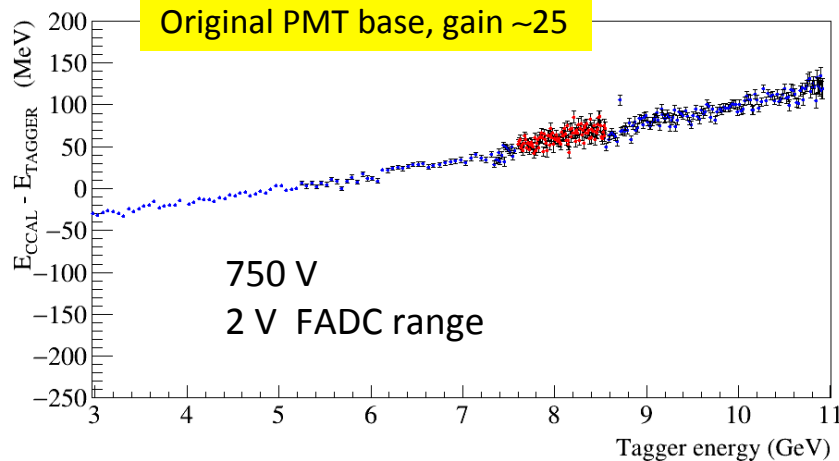
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Linearity

Linearity of the FADC peak amplitude



Amplifier circuit is designed on discrete high frequency transistors and it is similar to previously published at [2] circuit. Amplifier gain is about 10 and maximum linear pulse output amplitude is about 5V on 50 Ω load. This amplifier serve to compensate gain reduction at lower PMT operating voltage and allowed system operation with 10 times lower anode current without loss of overall gain and output amplitude see.

Some differences
with this paper

**New Photomultiplier Active Base for Hall C
Jefferson Lab Lead Tungstate Calorimeter**

¹Vladimir Popov, ²Hamlet Mkrtchyan

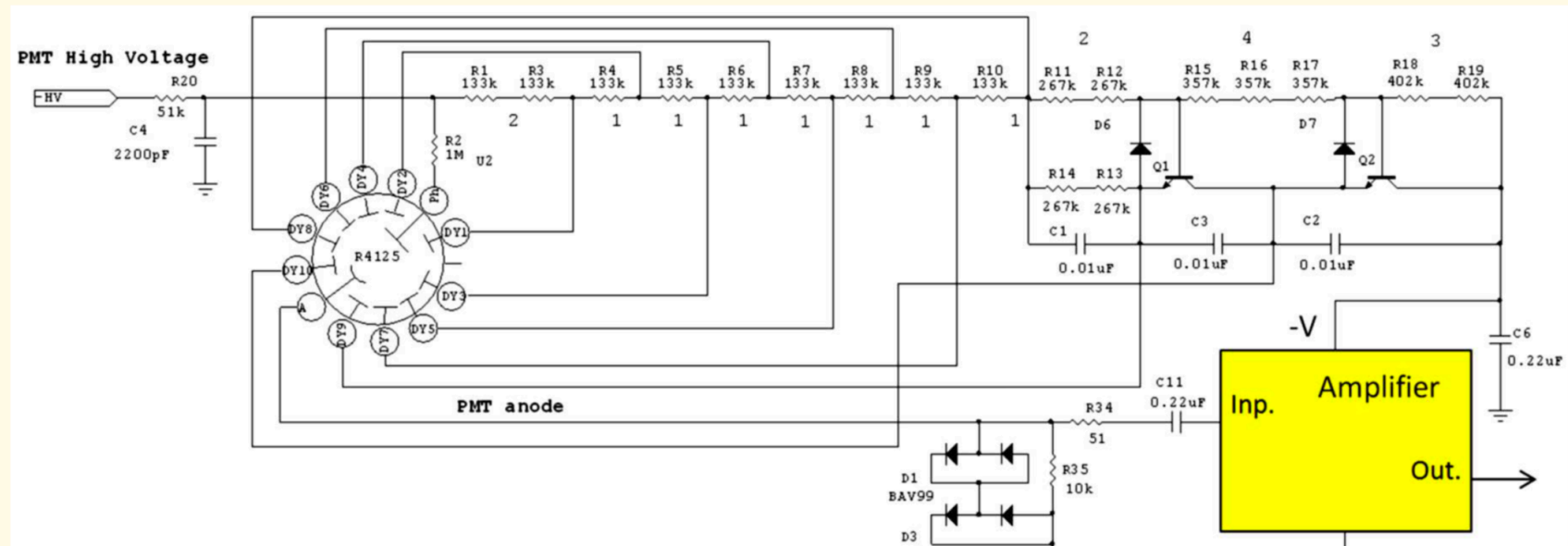
Conclusions +

- HV divider is not obvious
- Total linearity is a concern
- The anode current is a concern

Active base paper

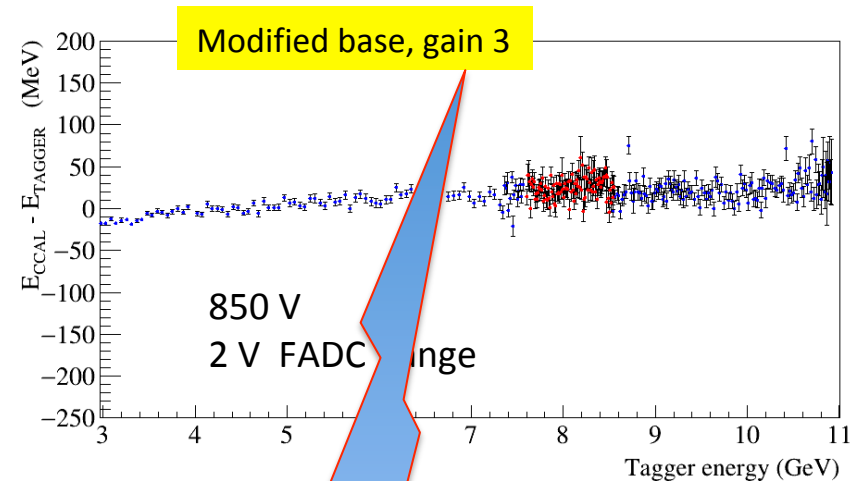
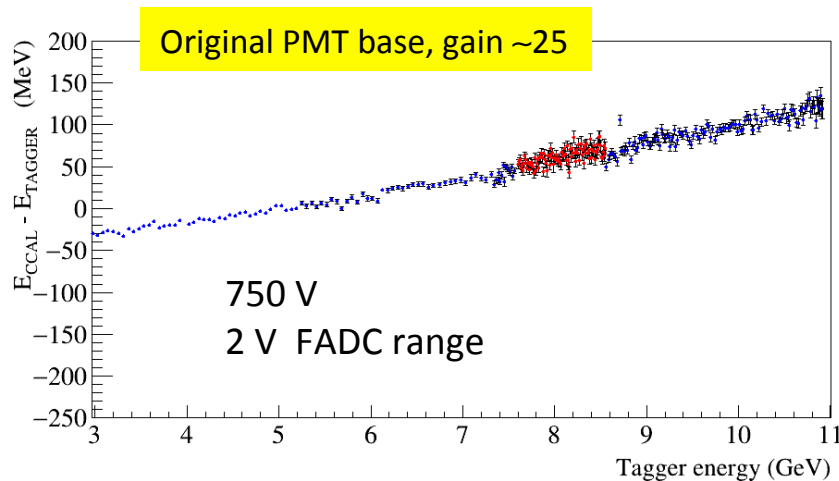
II. ACTIVE BASE CIRCUIT OVERVIEW

R4125 is a round shape, 19mm in diameter Hamamatsu photomultiplier tube. With gain about $8.7E+5$ at 1.5kV max. anode voltage, and rise time 2.5ns. New photomultiplier base is designed with the same as PrimEx experiment base voltage distribution ra-



Linearity

Linearity of the FADC peak amplitude



- Some non-linearities on the level of 2 – 3 % in the calorimeter response were observed for the original PMT base for both the peak amplitude and pulse integral
 - PMT was operated at relatively small HV, recommended HV is about 1 kV
- The linearity can be improved by reducing the amplifier gain and increasing HV. Some tuning of the PMT base may be required

Is it a low gain amplifier. Why to use it?

PMT handbook

The Photomultiplier Handbook

A. G. Wright

13.8.4 Shorting dynodes

Shorting dynodes is considered when it is discovered that light levels are higher than expected and a given PMT has too many stages. The possible consequences of operating at low gain, and hence low interdynode voltages, are a sluggish time response, gain that is sensitive to small changes in HV, and poor linearity. The best advice is to replace the PMT with one of fewer stages; the alternative is to short a set of consecutive dynodes to the anode. This may prove to be the only option, since the available choice of PMTs with fewer than six stages is very limited.

The configuration in Fig. 13.31(a) is customarily adopted, although it is the least desirable way of reducing the number of active dynodes, regarding linearity and speed of response. The arrangement in Fig. 13.31(b) attempts to mimic a

PMT handbook

Methods and circuits 509

