# Status of Research program with 26 simulations to be done in June.

"In order to **evaluate the CPS model** that you propose for KLF, I would like to see the results of simulations with various test configurations. For each configuration I would like to have the files for the **power depositions** (~4+ weeks, "fast" model, mesh-statistics) to estimate the **temperatures** just in the absorber, and I also would like you to present the **prompt and residual dose** environment in the **tagger hall** for **each of them (~13 weeks of calculations, "slow" model)**. The test configurations would be the following:"

- 1. Nominal configuration with FWHM=2.5mm in both x and y of the gaussian beam, and 10% radiator, and nominal magnetic field.
- 2. Beam transverse FWHM=0.8mm in both x and y direction. (?) Temperature is obviously higher.
- 3. 90% nominal magnetic field. (!) Linear dependence-nominal conf. as a 2nd point- of max energy deposition  $=> \pm 10\%$  change in max. temperature)
- 4. 110% nominal magnetic field (?) Linear dependence of max energy deposition  $= \ge \pm 10\%$  change in max. temperature
- 5. +1mm parallel shift in y for the beam transverse position. (!) Linear dependence. Criterion for a beam interlock system?
- 6. -1mm parallel shift in y for the beam transverse position.
- 7. Either +1mm or -1mm shift in x for the beam transverse position. (!) Not prevented by a beam trip system?
- 8. +0.5 mrad angle with respect to the nominal direction in Y (either just before or after the corrector magnet is fine). (?) similar to +25% B-field change.
- 9. -0.5 mrad angle with respect to the nominal direction in Y (either just before or after the corrector magnet is fine). (?) similar to 25% B-field change.
- 10. Either +0.5 mrad or -0.5 mrad angle with respect to the nominal direction in X (either just before or after the corrector magnet is fine).(!)
- 11. Beam transverse FWHM=3.5mm in both x and y. (?) obviously lower temperature, (!) higher background at the CPSentry
- 12. Beam halo as a flat background distribution under the main gaussian peak of the beam extending radially 0.5cm from the center of the beam at the relative level of 10<sup>-4</sup> with respect to the gaussian peak height with FWHM=2.5mm in both x and y. (!)
- 13. 20% radiation length for the copper radiator before CPS. (!) (Lower temperature, higher photon beam intensity, same background).

## • 13 simulations for the Temperature estimates are done with 20 s/primary.

Background and Activation simulation rate is of 100 s/primary.

### Power Deposition map around the beam channel at 90 < z/cm < 160



Power Deposition Density W/cm<sup>3</sup> bentcoil-65-m23absrad20 99

• dP/dV(z) is shown at the next two slides

### Power deposition in Hot Spot for 8 (13) configurations. B=80%B<sub>nom</sub>, $\Delta \phi = 1/40$ , $\Delta r = 0.025$ cm.



#### Power deposition in Absorber Hot Spot for 5 (13) beam configurations. $\Delta \phi = 1/40$ , $\Delta r = 0.025$ cm



# Research program for the background simulations for June (optimized?)

- Background map is defined by energy deposition profile dE/dz.
- 0.5 mrad e-beam walk translate to 5.E-4\*7000 cm=3.5 cm of photon beam walk at KPT. Looks like too much (10 times?) for a photon beam interlock. Seems may be excluded(?).
  - 1. Reference 4 days (with 12 clones)
  - 2. Halo r<0.5 cm 4 days
  - 3. y=y-1 High radiation upstream CPS; dE/dz is similar to 110%B -4 days.
  - 4. y=y+1 High radiation downstream CPS?; dE/dz is similar to 90%B 4 days.

• Seems may be done by June 22.

# Comments to the video. What is the wedge effect?

- 1) Consider e-**beam as a cylinder diameter D** with uniform density; direction  $\mathbf{n}_{\mathbf{b}} = (0, \sin(\alpha), \cos(\alpha))$ , where  $\alpha$  pitch angle to the beam axis.
- 2) For a squared or wedge-like channels the hot spot is a cross section of a cylinder with a plane. Plane orientations:  $\mathbf{n_1} = (0,1,0)$  -for squared channel, or  $\mathbf{n_2} = (\pm \cos(\varphi), \sin(\varphi), 0)$  - for 2 wedge planes obtained as  $\pm \varphi$  - rotation of yz-plane around z-axis.

Impact angle is determined by  $(\mathbf{n}_{\mathbf{b}}, \mathbf{n}_{\mathbf{1}}) = \sin(\alpha)$  or  $(\mathbf{n}_{\mathbf{b}}, \mathbf{n}_{\mathbf{2}}) = \sin(\alpha)\sin(\varphi) = \sin(\vartheta)$  - pitch to wedge plane.

- 3) But in both cases the **intersection is an ellipse** with the area  $S = \pi D \times L$ , where L ellipse large axis.
- 4) Pitch angle  $\vartheta \sim D/L$ .
- 5) Maximum **L** is constrained by the length of the beam channel (L<L<sub>c</sub>~2 m), or the wedge (L<L<sub>w</sub>~0.5 m).
  - Therefore max  $dP/dS \propto \vartheta \propto L^{-1}$  for the wedge is  $L_c/L_w = 4$  times higher.



- Effect of rotated squared channel is of 20% to lower maximum energy deposition!
- Advantage: transverse dimensions 1 cm ×1 cm !!!



# Optimisation of Tim Whitlatch (TW) design at 90% nominal B-field. Absorber Channel "stingray" D=10 mm. Power Deposition.



- Maximum power deposition 1.6 kw/cm<sup>3</sup>; r/cm<0.025; -0.0125<φ<0.0125 (1/80).
- Lower temperature -> higher photon beam.
- Allows standard photon beam walk in x or y within 1 cm.
- Equivalent to lower magnetic field.

# Optimisation of Tim Whitlatch design at 70% B-field. Absorber Channel rhombus D=10 mm. Power Deposition.



0.7 0.6 0.5 0.4 0.3 0.2 0.1 0.5 0.1 -0.2 -0.3 -0.4 -0.5 -0.

- Maximum power deposition is of 1.4 kw/cm^3 r/cm<0.025 -0.0125<fi<0.0125
- B to be increased up to 0.90% of nominal magnet field.