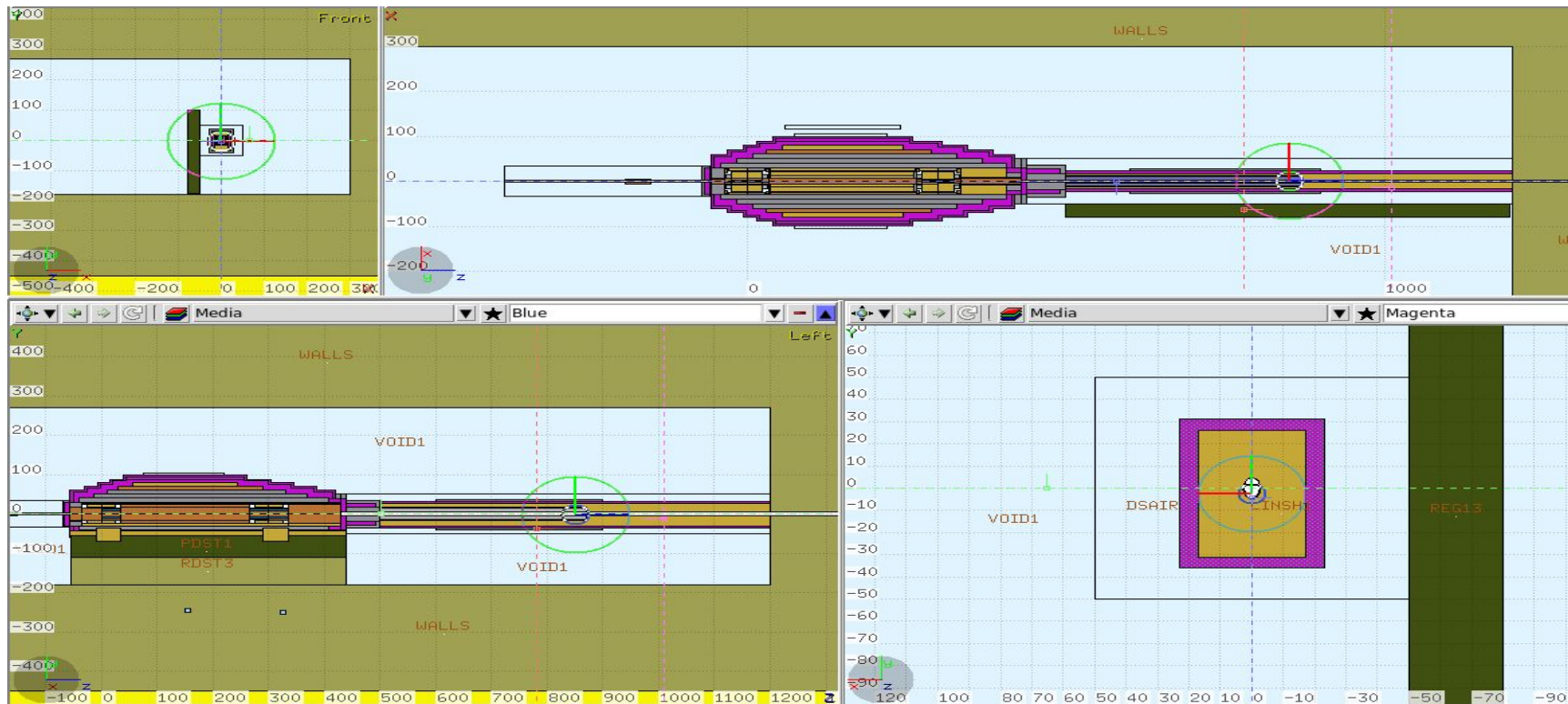


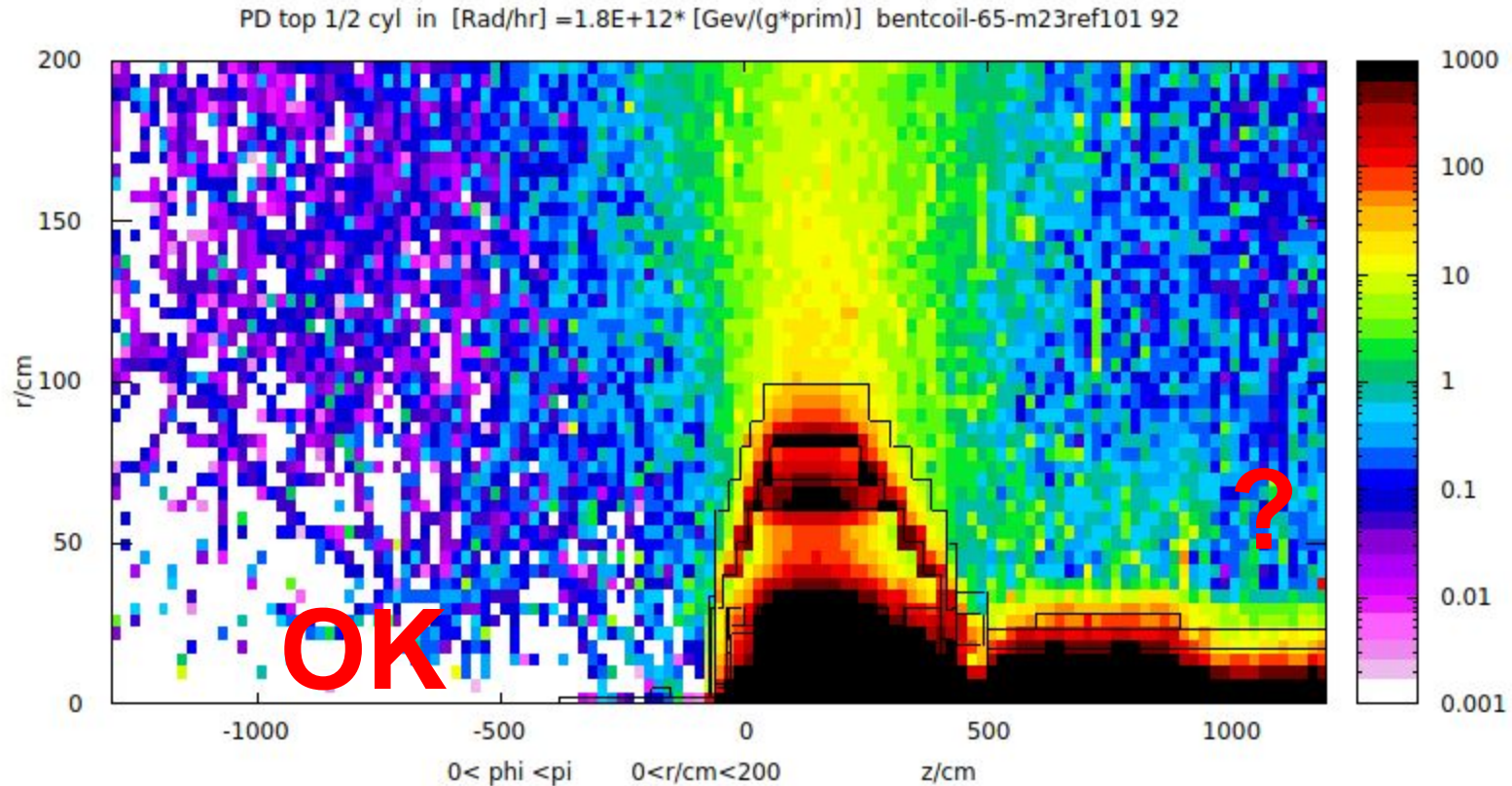
CPS beam line and VBV lifetime; Teflon as a benchmark.

[baturin@hallal1 ABSTSTref9]\$ flair bentcoil-65-m23ref101.flair

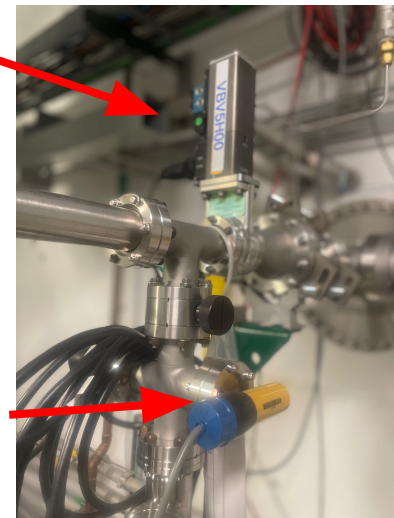
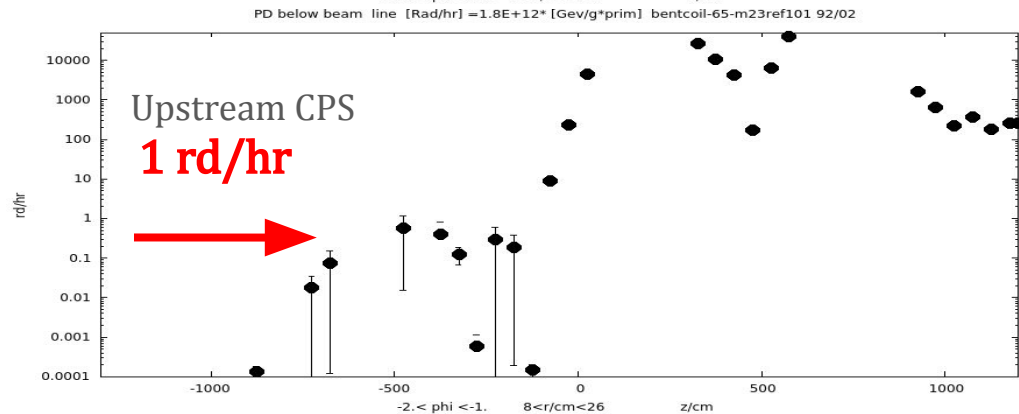
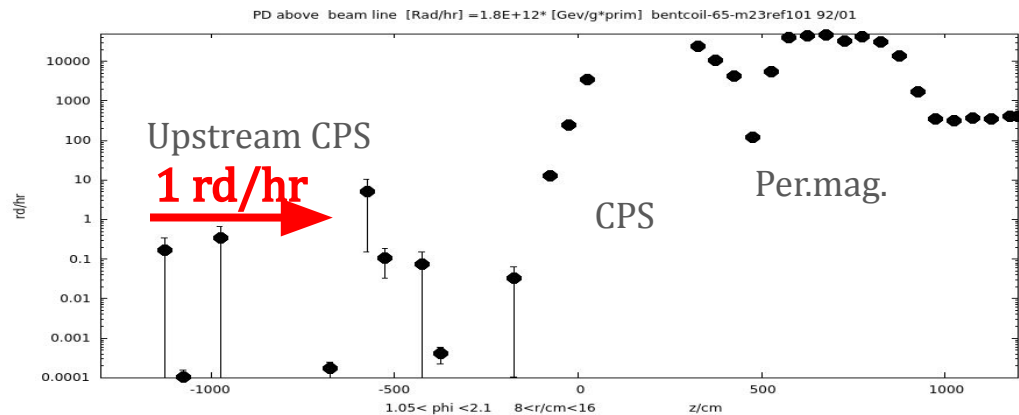


- Assume that critical part of vacuum remote control (VBV) is located at $8 < r / \text{cm} < 16$
- What is PD in this area along the beam line? What is neutron flux - to be respon.

Prompt Dose r.vs.z -profile above the beam line (top 1/2 semi sphere).

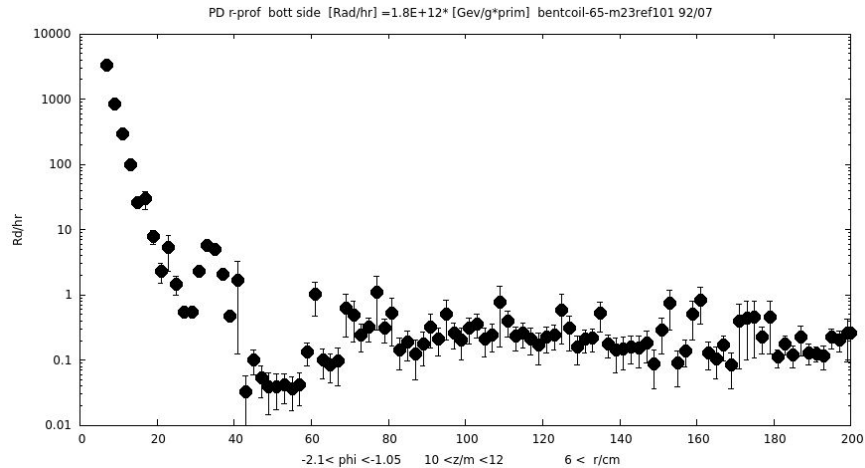
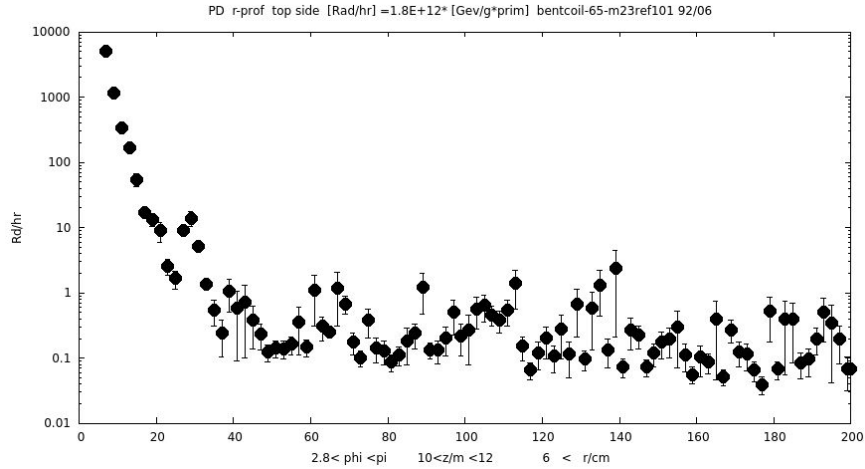


Prompt Dose z-profile on Top and Bottom of the beam line at $8 < r/cm < 16$



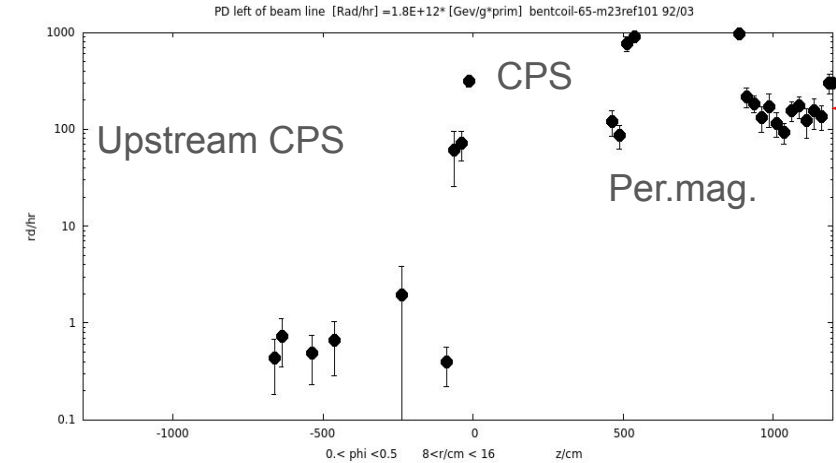
- Place upstream CPS with Bypass line?

Prompt Dose r-profile on Top and Bottom of the beam line. $10 < z/m < 12$



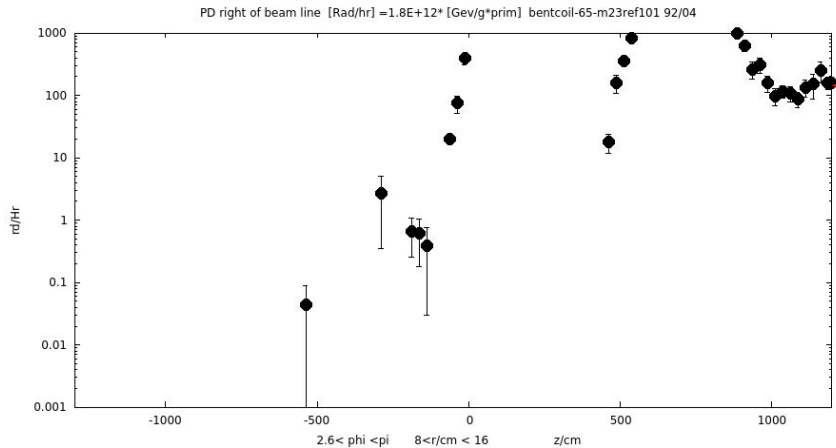
- At $r/cm = 8$ PD = ~ 1000 rd/hr
- At $r/cm = 14$ PD = ~ 100 -200 rd/hr
- At $r/cm = 20$ PD = ~ 2 rd/hr
- At $r/cm > 30$ PD = ~ 10 rd/hr

PD z-profile Left and Right to the beam line at $8 < r/\text{cm} < 16$



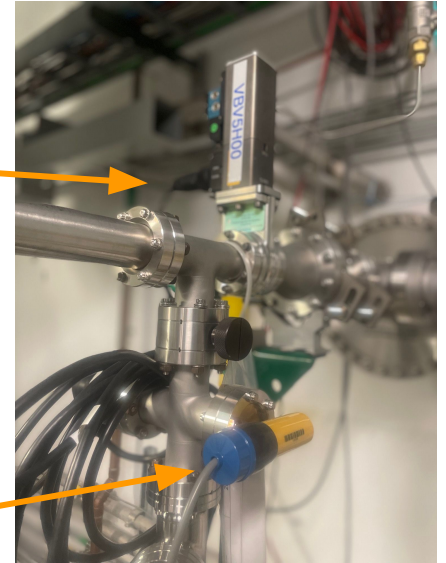
150 rd/hr Left side

r=8 cm



150 rd/hr

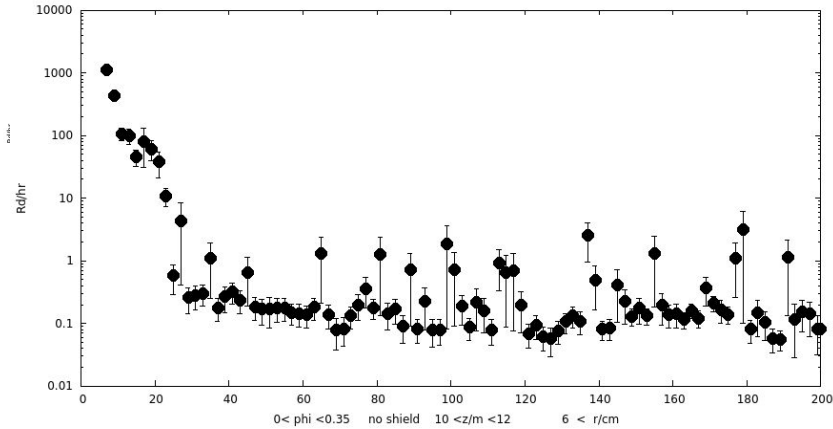
r=16 cm



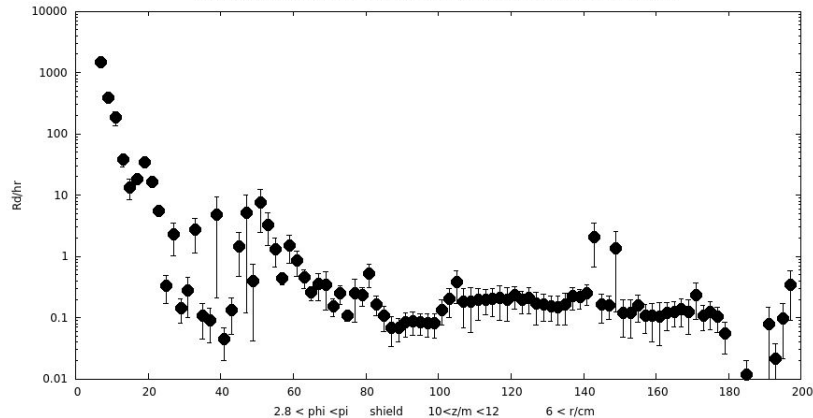
- Lower than for Top and Bottom due to orientation of permanent magnet.
- Change orientation by 90° ?

PD r-profile. Left and Right to the beam line. $10 < z/m < 12$

PD r-profile left side [Rad/hr] = $1.8E+12$ [Gev/g*prim] bentcoil-65-m23ref101 92/09



PD r-prof right side [Rad/hr] = $1.8E+12$ [Gev/g*prim] bentcoil-65-m23ref101 92/08



- At $r/cm = 8$ **PD = ~ 500 rd/hr !**
- At $r/cm = 14$ PD = $\sim 50-100$ **rd/hr**
- At $r/cm = 30$ PD = ~ 0.1 rd/hr !
- Left=right difference is due to the additional concrete shield at the right side
- Twice lower than for Top and Bottom profiles.

Tensile strength of Teflon (pPTFE 6.4×50.1 mm) vs TID **in Air**.

<https://www.sciencedirect.com/science/article/pii/014139109290093K?via%3Dihub>

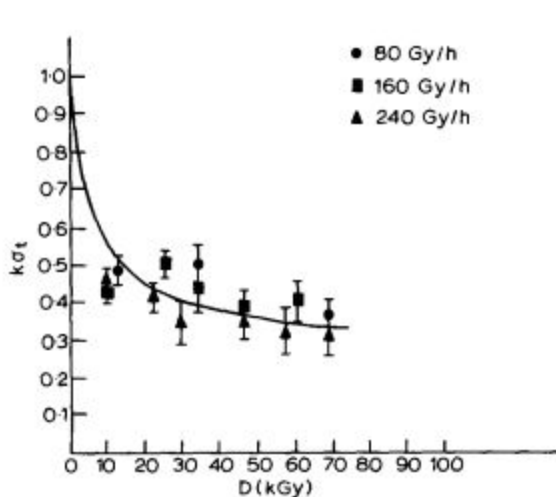


Fig. 3. The dependence of $K_{\sigma t}$ on the doses, D , for pPTFE irradiated at various dose rates (80 Gy/h, 160 Gy/h, 240 Gy/h).

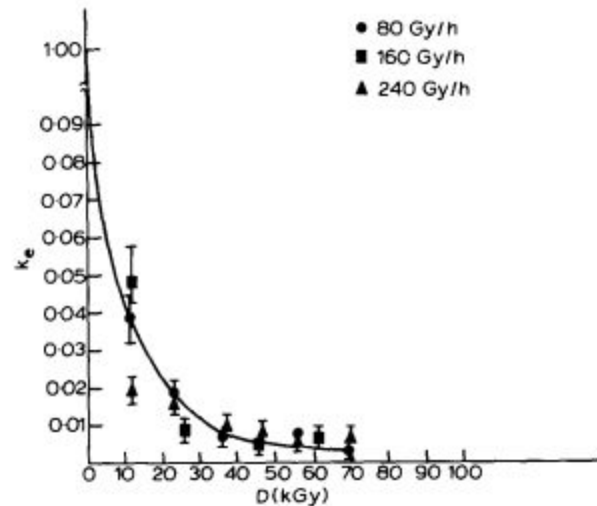


Fig. 6. The dependence of K_e on the dose, D , for pPTFE irradiated at various dose rates (80 Gy/h, 160 Gy/h, 240 Gy/h).

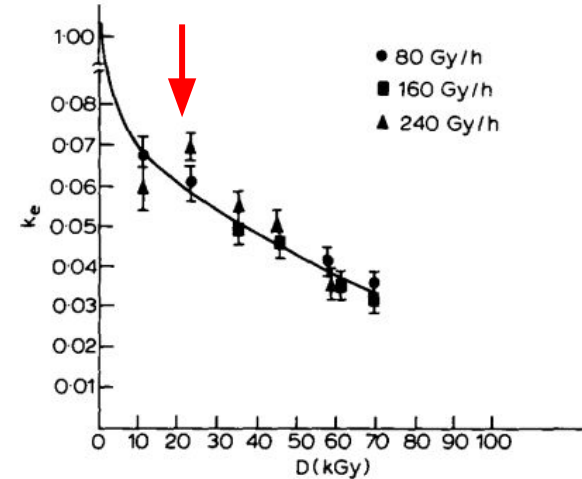
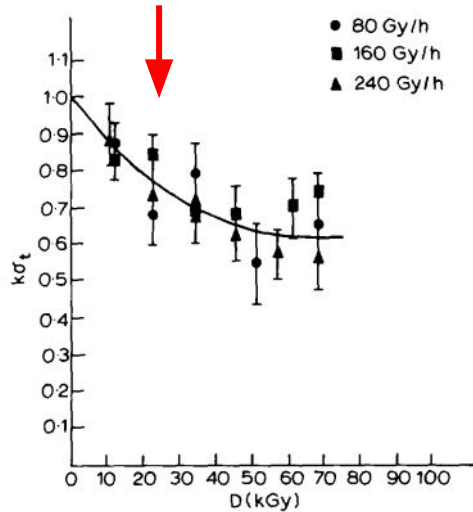
- At 20.E+3 Gy= **2 Mrad** (up to **10 Mrad**?) pure Teflon sample brakes at $\sim 45\%$ of nominal load, elongates by $\sim 2\%$.
- At 100 rad/hr (of γ) Teflon LT = 2.E+4 hrs = 2.3 years. May be 3 times longer - 7 years!

Tensile strength of Teflon (cPTFE 6.4×50.1 mm) vs TID in Air.

<https://www.sciencedirect.com/science/article/pii/014139109290093K?via%3Dihub>

<https://www.osti.gov/servlets/purl/1671997>

M. I. Chipară



Ratio of “tensile strength” of irradiated and unirradiated samples of cPTFE (Carbon filled) vs TID/kGy .

Ratio of the “elongation at break” for irradiated to that of unirradiated cPTFE vs TID/kGy.

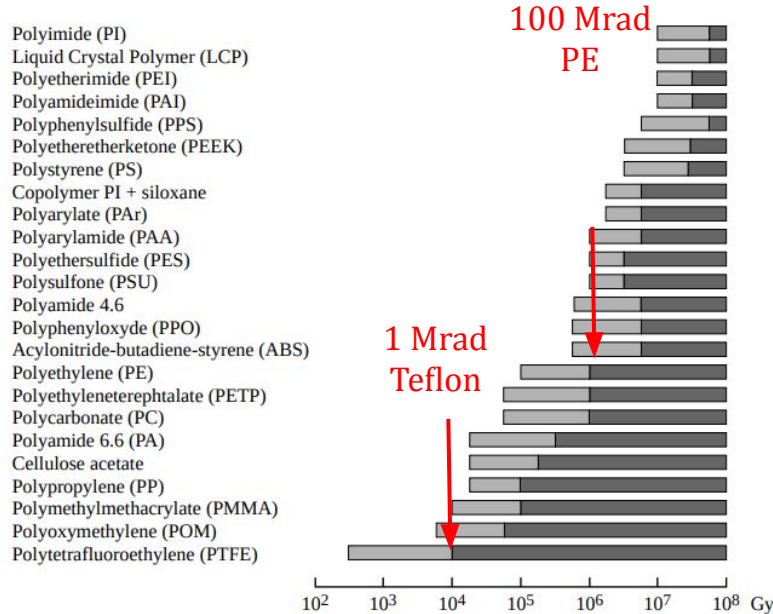
- At 20.E+3 Gy= **2 Mrad** Teflon+C sample Brakes at $\sim 80\%$ of nominal load, while elongates by $\sim 6\%$.
- At 100 rad/hr (of γ) Teflon LT = 2.E+4 hrs = 2.3 years.

Compilation of Radiation Damage Test Data

<https://cds.cern.ch/record/357576/files/CERN-98-01.pdf>

Table 2a

General classification of rigid thermoplastics with respect to their radiation resistance





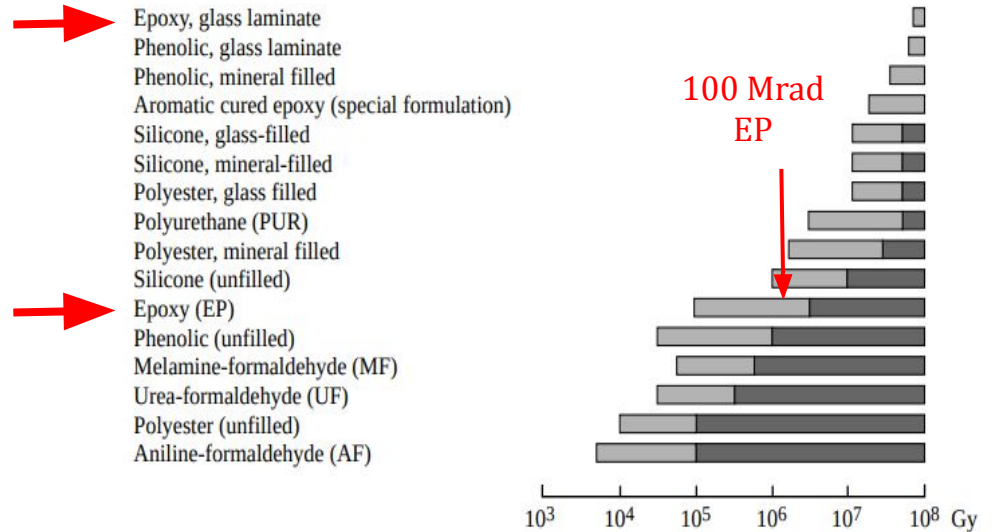


 mild to moderate damage, utility is often satisfactory
 moderate to severe damage, use not recommended

Table 2b

General classification of thermoset resins and composites with respect to their radiation resistance



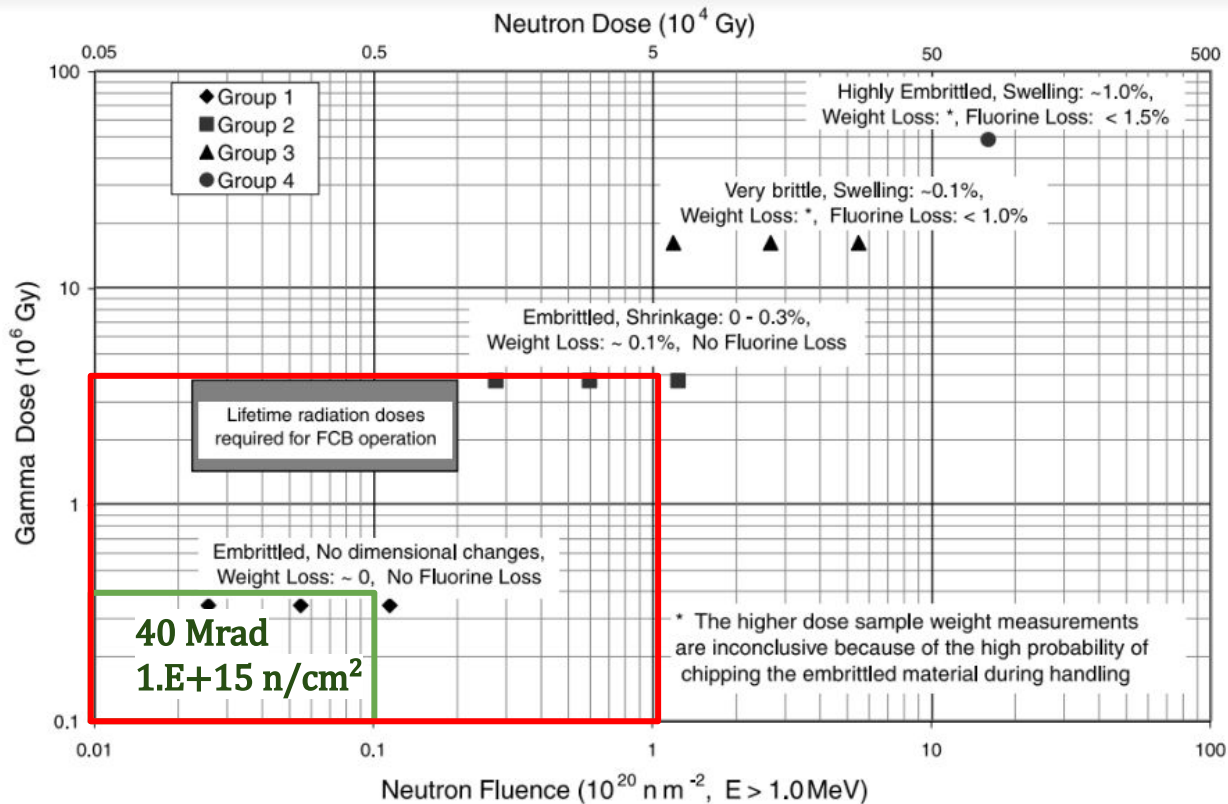
 mild to moderate damage, utility is often satisfactory
 moderate to severe damage, use not recommended

Irradiation performance of PolyTetraFluoroEthylene (PTFE, Teflon, $0.6^2 \times 10 \text{ cm}^3$) in a mixed fast neutron and gamma radiation field.

Otto K. Harling *, Gordon E. Kohse, Kent J. Riley

MIT Nuclear Reactor Laboratory, 138 Albany Street, Cambridge, MA 02139, USA

Received 17 December 2001; accepted 1 April 2002



Teflon tests were done in Air atmosphere!

- Critical Prompt Dose $\sim 10-40 \text{ Mrad}$
- Critical neutron flux $\sim 1.E+15 \text{ n/cm}^2$

Fig. 1. Summary of the PTFE irradiation tests.

HEATING ELEMENT

BASE MATERIAL: Teflon

TYPE: -

SUPPLIER: -

IDENTIFICATION: 291-1980

DESCRIPTION OF MATERIAL:

Flexible heating element of total width 68 mm consisting of a carbonized tissue (woven fibres) of width 38 mm embedded in an insulating coating of Teflon

APPLICATION AT CERN:

Heating element for vacuum chamber bakeout at the Intersecting Storage Rings and at the Super Proton Synchrotron LSS4 and LSS5

IRRADIATION CONDITIONS:

Type: Reactor ASTRA, switched-off reactor position 35 in air, dose rate 10 Gy/s

Doses: 1×10^5 , 1×10^6 Gy

METHODS OF TESTING:

RESULTS:

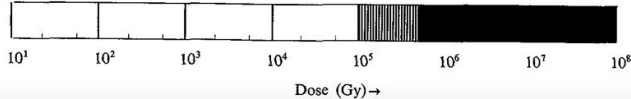
Teflon matrix was severely damaged at 1×10^6 Gy. After some handling to test flexibility, the electrical resistance was greater than $2 \times 10^6 \Omega$. At the lower dose of 1×10^5 Gy, however, the Teflon did not break, and the electrical resistance was $6.6 \times 10^3 \Omega$ at a length of 15 cm.

Remarks:

REFERENCES:

APPRECIATION: *****USE IN HIGH LEVEL RADIATION AREAS NOT RECOMMENDED*****

See Appendix 7

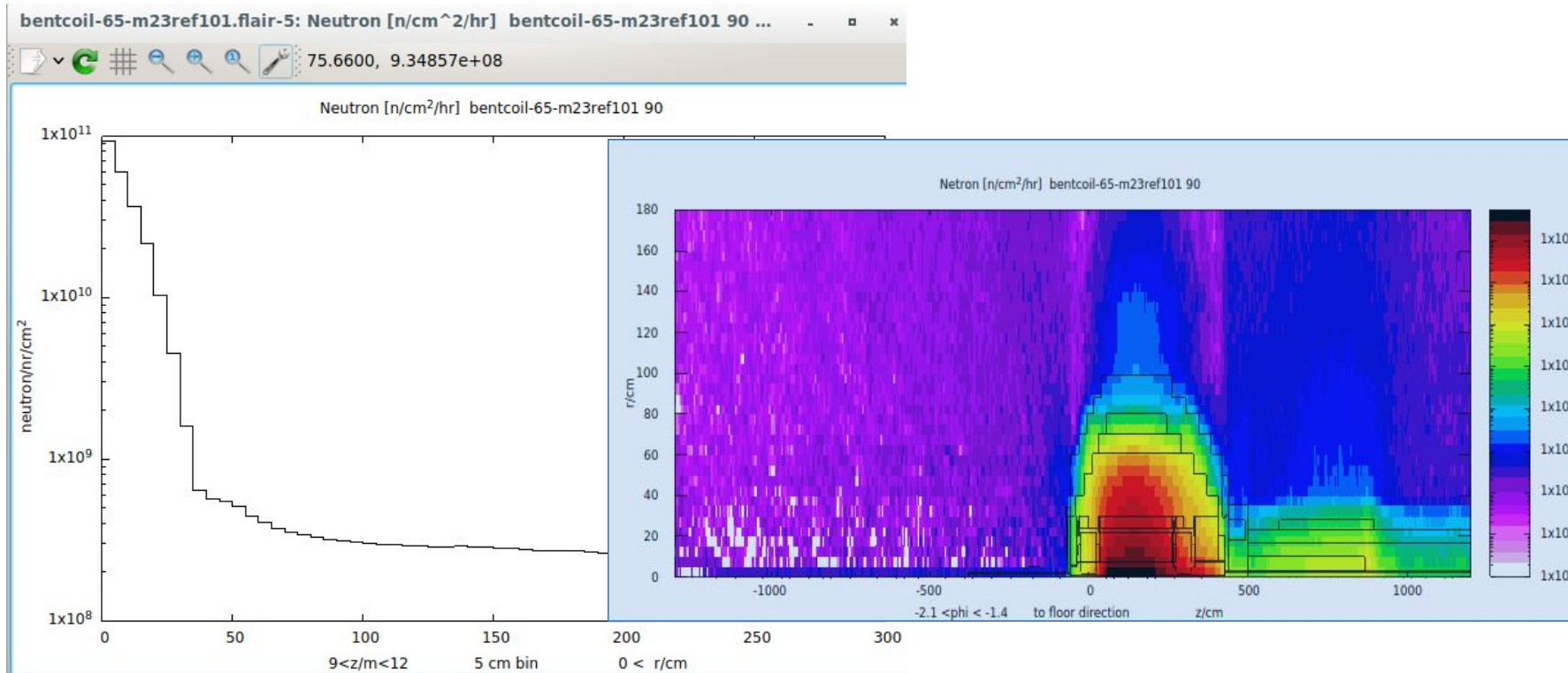


CERN compilation of radiation damage data (1980)

Teflon in a heating element. Test in Air!

- Teflon **does not break** at $1.E+5$ Gy = **10 Mrad !**

Teflon LT and Neutron flux r-profile near exit form Tagger Hall ($9 < z/m < 12$)



- At $10 < r/cm < 15$ neutron flux $\sim 0.4 \text{ E}+11 \text{ n/cm}^2/\text{hr}$; maximum PD=500 rad/hr
- **Neutron**-induces Teflon LT $> 20000 \text{ hrs} = \sim 2 \text{ year}$ (critical flux = $1 \cdot \text{E}+15 \text{ n/cm}^2$)
- **Photon** - induced Teflon LT $> 10 \text{ Mrad}/500\text{rad/hr} = 20000 \text{ hrs} = \sim 2 \text{ years}$ (critical PD = 10 Mrad)

ELECTRONIC COMPONENTS

BASE MATERIAL: Various

TYPE: See table below

SUPPLIER: Various

IDENTIFICATION: 133-1974

CERN compilation of radiation damage data (1980)

Stable operation of electronic components

Integrated

TTL logics, amplifiers, General purp. Si $1.E+13 \text{ n/cm}^2$. (200/2000/20000 hrs)

Diodes

General purpose Si $1.E+13 \text{ n/cm}^2$. (200/2000/20000 hrs)

Ht Carrier, Zener $1.E+14 \text{ n/cm}^2$. (200/20000/20000 hrs)

Resistors

Carbon and wire $1.E+14 \text{ n/cm}^2$. (2000/20000 hrs)

Metal Film unlimited

Capacitor

Ceramic $1.E+13 \text{ n/cm}^2$ (200/2000/20000 hrs)

Polyester $1.E+14 \text{ n/cm}^2$ (2000/20000 hrs)

Mica, MKL, Tantalum unlimited

All brakes typically at 10 times higher neutron flux.

AT $10 < r/cm < 15$ neutron flux $\sim 0.5 E+11 \text{ n/cm}^2/\text{hr}$.

At $25 < r/cm < 30$ -/- $\sim 0.5 E+10 \text{ n/cm}^2/\text{hr}$

At $50 < r/cm$ -/- $\sim 0.5 E+09 \text{ n/cm}^2/\text{hr}$

Designation	Type	Exposure in n/m^2 ($E > 1 \text{ MeV}$ *)				
		10^{16}	10^{17}	10^{18}	10^{19}	
Resistor:	carbon	1 kΩ, 5%	██████████	██████████	██████████	
	metal film	1 kΩ, 1%	██████████	██████████	██████████	
	wire wound	100 Ω, 5%	██████████	██████████	██████████	
Capacitor:	potmeter "cermet"	1 kΩ, 78P	██████████	██████████	██████████	
	ceramic	20 nF, 30 V	██████████	██████████	██████████	
	mica	22 pF, 300 V	██████████	██████████	██████████	
	polyester	15 nF, 125 V	██████████	██████████	██████████	
	polycarbonate	15 nF, 250 V	██████████	██████████	██████████	
	MKL	0.22 μF, 100 V	██████████	██████████	██████████	
Diode:	electrolytic Al	200 μF, 10 V	██████████	██████████	██████████	
	tantalum	15 μF, 20 V	██████████	██████████	██████████	
	rectifier, Si	10D6	██████████	██████████	██████████	
	general-purpose, Si	1N914	██████████	██████████	██████████	
	hot carrier, Si	BAV72	██████████	██████████	██████████	
	Zener, Si	HP2900	██████████	██████████	██████████	
	tunnel, Ge	ZF6,8	██████████	██████████	██████████	
	Transistor:	NPN, Si	1N3717	██████████	██████████	██████████
		PNP, Si, rad. resist.	2N918	██████████	██████████	██████████
		FET, Si, N-channel	2N5332	██████████	██████████	██████████
FET, Si, P-channel		MM4261H	██████████	██████████	██████████	
MOSFET, P-channel		2N3819	██████████	██████████	██████████	
MOSFET, N-channel		2N3820	██████████	██████████	██████████	
Integrated:		TTL gate	3N165	██████████	██████████	██████████
		TTL flip-flop	BSV81	██████████	██████████	██████████
		TTL counter	SN7400N	██████████	██████████	██████████
		TTL one-shot	SN7473N	██████████	██████████	██████████
		TTL gate	SN7493N	██████████	██████████	██████████
		TTL flip-flop	SN74121N	██████████	██████████	██████████
	amplifier, rad. res.	MC3000P	██████████	██████████	██████████	
	amplifier, rad. res.	MC3055P	██████████	██████████	██████████	
	op. amplif. rad. res.	RSN55900	██████████	██████████	██████████	
	op. amplif. rad. res.	RSN55910	██████████	██████████	██████████	
	op. amplif. rad. res.	RSN52709	██████████	██████████	██████████	
	op. amplif. FET input	μA744	██████████	██████████	██████████	
	op. amplif. gen. purpose	μA740	██████████	██████████	██████████	
	comparator	MC1741	██████████	██████████	██████████	
	op. amplif.	SN72710	██████████	██████████	██████████	
	op. amplif.	T1303	██████████	██████████	██████████	
	op. amplif. FET input	T1319	██████████	██████████	██████████	
	Discrete:	op. amplif.	T1420	██████████	██████████	██████████
DAC, 10 bits		T1024	██████████	██████████	██████████	
Rectifier:	selenium	T4022	██████████	██████████	██████████	
		B250C75	██████████	██████████	██████████	

*) Conversion factor $10^{17} \text{ n/m}^2 (E > 1 \text{ MeV}) \approx 410 \text{ Gy}$ in organic (CH_2) materials or 12 Gy in silicon.

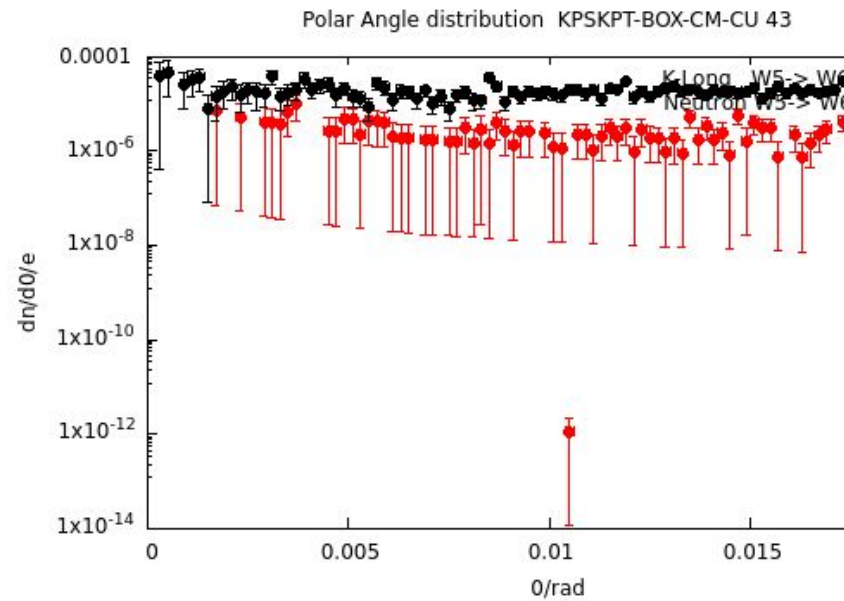
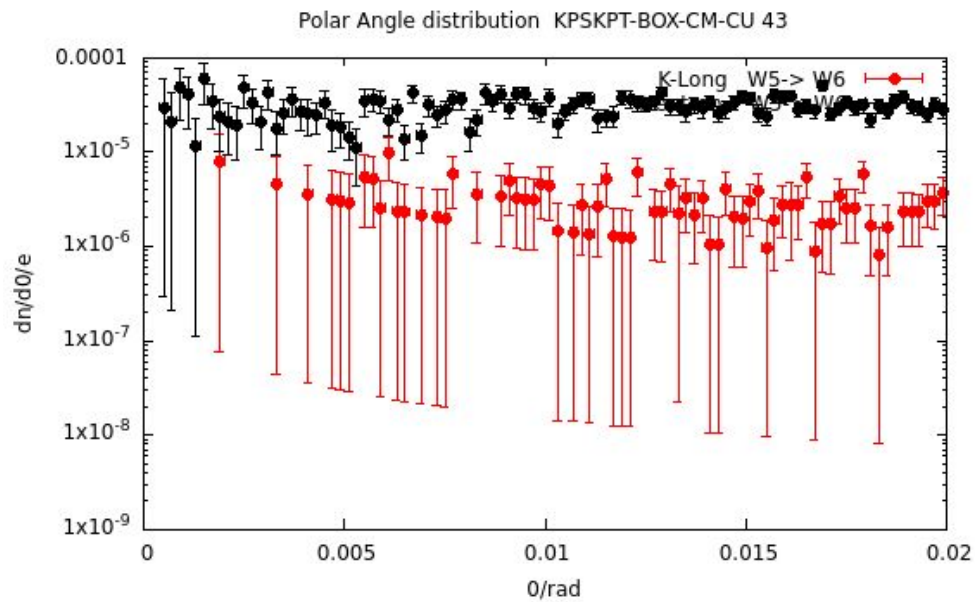


CONCLUSION

Teflon at $r = 8$ cm ; worst case scenario.

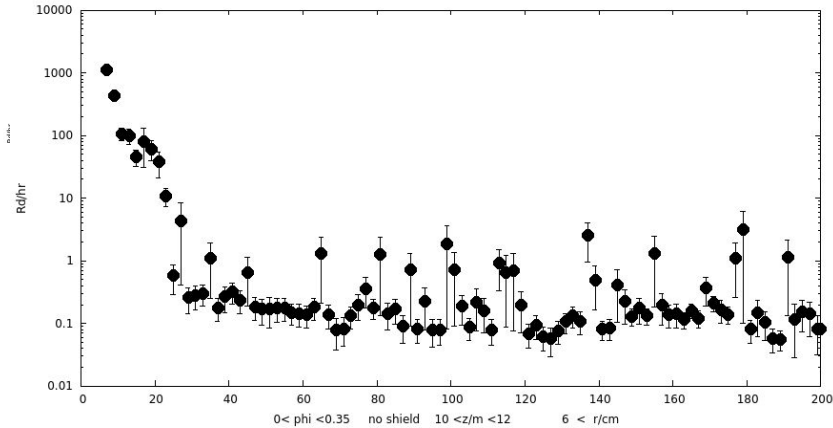
- **VBV cable** at the exit from Tagger Hall ($10 < z/m < 12$) is exposed to ~ 500 rad/hr (at $r = 8$ cm).
- From **CERN** database, and Slide-8, we read for the **Teflon** TID = **2 Mrad** (up to 40 Mrad). Therefore,
- Under **photons** **Teflon** **LT = 0.5 years** (up to 10) of continuous operation (~ 170 days = $4.E+3$ hrs ; SHV conn.).
- Under **neutrons** Teflon **LT = 2 years**
- **Epoxy** and **Polyethylene** **LT = 50 years** (20000 days = $\sim 4.E+5$ hrs, PCBs and cable insulation).
- At the upstream side of the beam line all **LTs** are ~ 100 times longer.
- Is it possible to **avoid** placing **vacuum equipment downstream** the CPS using bypass line?
- Engineering solution to avoid vibration and mechanical load on SHV connectors.

- From **exponential r-profiles** \Rightarrow at $r = \sim 15$ cm LTs are ~ 10 times longer.
at $r = \sim 30$ cm — ~ 100 times longer

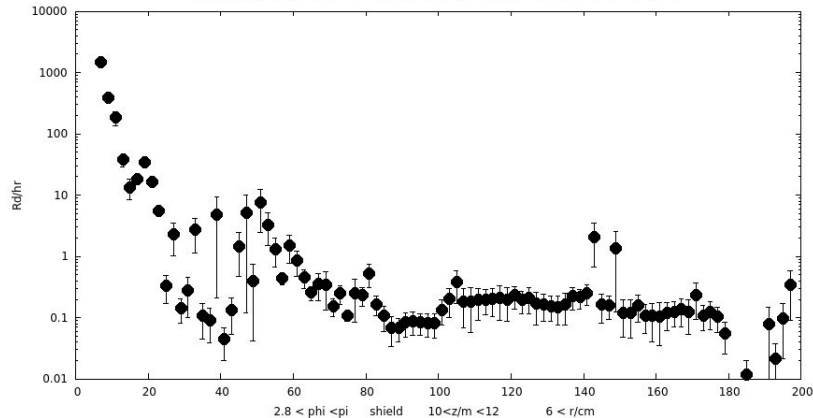


PD r-profile. Left and Right to the beam line. $10 < z/m < 12$

PD r-profile left side [Rad/hr] = $1.8E+12$ [Gev/g*prim] bentcoil-65-m23ref101 92/09



PD r-prof right side [Rad/hr] = $1.8E+12$ [Gev/g*prim] bentcoil-65-m23ref101 92/08



- At $r/cm = 8$ PD = ~ 500 rd/hr !
- At $r/cm = 14$ PD = $\sim 50-100$ rd/hr
- At $r/cm = 30$ PD = ~ 0.1 rd/hr !
- Left=right difference is due to the additional concrete shield at the right side
- At $r=14$ twice lower than for Top and Bottom profiles.