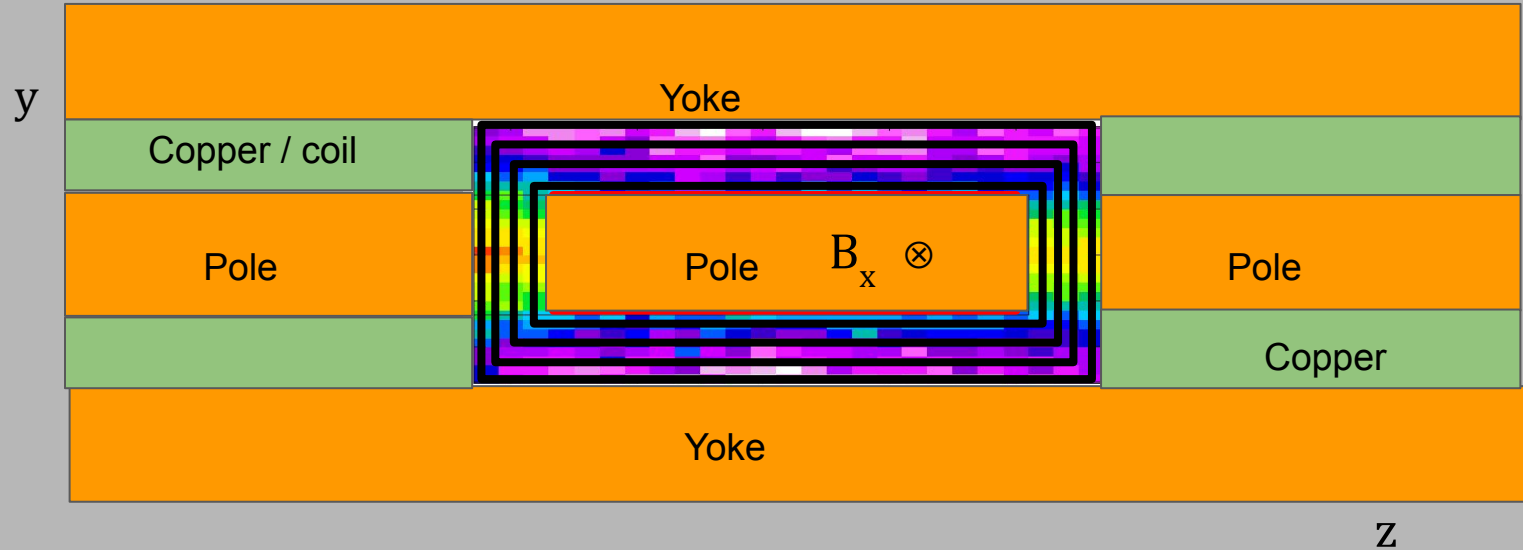
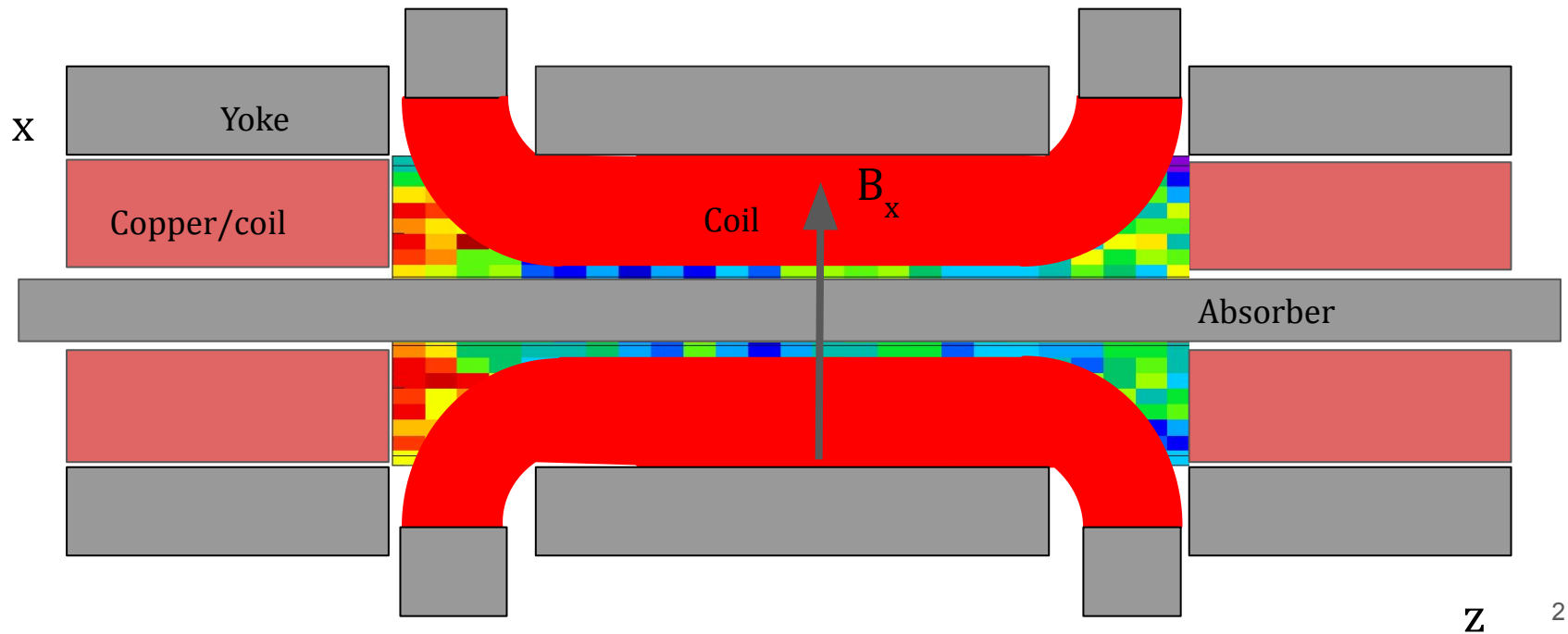


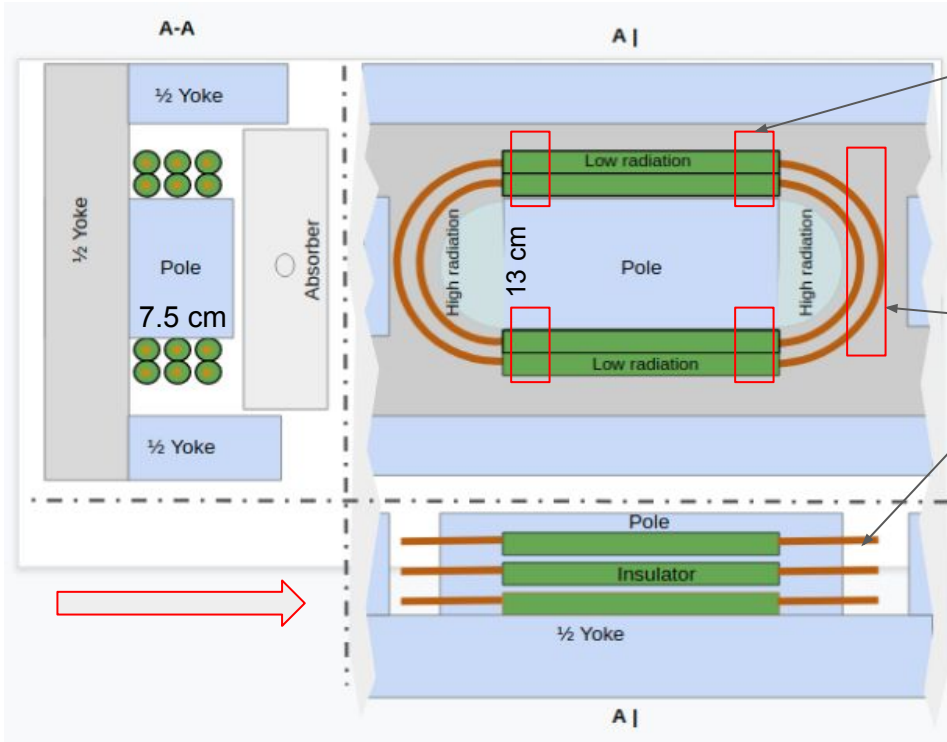
Problem of High radiation in return part of Coils.



Tim Whitlatch's solution.



Coil Design and Insulation Exposure to Radiation.



Hot area for insulation.

Very hot area,
Air insulation,
Gap between
wires
~8 mm.

Ampere's force law:

$$dF/dl = (\mu_0 / 2\pi) (I^2/d) = \sim 25 \text{ N/m}$$

at $I=1800 \text{ A}$; $d=2.5 \text{ cm}$; $\mu_0 = 4\pi \times 10^{-7} \text{ N/A}^2$

- Attractive force of bent parts $F = 25 \text{ N/m} \times 0.3 \text{ m} = 7.5 \text{ N}$.
- Copper 1.7 cm -wires (tubes) will not touch .

Leakage Current between wires.

Current through gas :

$$dI/ds \text{ [A/cm}^2\text{]} = n \text{ [e/cm}^3\text{]} \times v \text{ [cm/s]} \times e \text{ [C]}$$

1. What is concentration of electrons n ?
2. What is the drift velocity of electrons v ?

1. What is n and Ionisation in Magnet Coil.

$$dI/ds [A/cm^2] = n [e/cm^3] \times v [cm/s] \times e$$

Assume **maximum dose D in space between coil windings** is $D = 1.E-5 [GeV/g/e]$ ($\sim 10 \times$ of **FLUKA** estimate).

Assume **10 eV** is required to produce one electron-ion pair.

Dose D translate to ion **pair production** $\sim 1.E+3 [pair/g/e] = 1.E-5 [GeV/g/e] / 1.E-8 [GeV]$.

Ion pair production rate **per unit of mass** is at beam intensity $3.E+13 [e/s]$:

$$dN/dt = 3.E+16 [pair/g/s] = 1.E+3 [pairs/g/e] \times 3.E+13 [e/s].$$

Assume we have **1 cm of argon** between windings ($\rho_A = 1.7E-3 [g\ cm^{-3}] = \sim 2.E-3$).

Air - $1.3E-3$; He - $0.17E-3$

So we find the ion **production rate between coil wires** :

$$dn_p/dt = (dN/dt) \rho_A = 3.E+16 [pairs\ g^{-1}\ s^{-1}] \times 2.E-3 [g\ cm^{-3}] = 6.E+13 [pair\ cm^{-3}\ s^{-1}]$$

This rate is **balanced by recombination** of argon ions and electrons.

1. What is n. Ionisation in Magnet Coil and Leakage Current.

$$dI/ds \text{ [A/cm}^2\text{]} = n \text{ [e/cm}^3\text{]} \times v \text{ [cm/s]} \times e$$

$dn_p/dt = 6.E+13 \text{ [pairs cm}^{-3} \text{ s}^{-1}\text{]}$ is balanced by recombination of argon ions and electrons defined as:

$$dn_r/dt = \alpha n_+ n_- , \quad \text{where } \alpha = 2.E-10 \text{ [cm}^3 \text{ i}^{-1} \text{ s}^{-1}\text{]} \text{ recombination coeff. for Argon.}$$

$$(\alpha = \sim 1.E-8 \text{ [cm}^3 \text{ i}^{-1} \text{ s}^{-1}\text{]} \text{ for He, and } \alpha = 1.E-6 \text{ — } 1.e-7 \text{ for Air.)}$$

Assuming equal densities $n_+ = n_- = n$ for the equilibrium density of electrons n we write:

$$\alpha n^2 = dn_p/dt = 6.E+13 \text{ [pairs cm}^{-3} \text{ s}^{-1}\text{]} \text{ from the previous slide and}$$

$$n^2 = \alpha^{-1} dn_i/dt = 0.5E+10 \text{ [pairs s cm}^{-3}\text{]} \times 6.E+13 \text{ [pairs cm}^{-3} \text{ s}^{-1}\text{]} = 3.E+23 \text{ (pairs/cm}^3\text{)}^2.$$

- The equilibrium density of electrons yields $n = 6.E+11 \text{ (pairs/cm}^3\text{)}.$
- Density of electrons is proportional to the gas specific factor $(\alpha^{-1} q_A)^{1/2}.$

2. What is v and Electric Field between Wires at 2 kA current.

What is Voltage between windings?

Copper resistivity $\kappa=1.7E-6$ [Ohm·cm]; $L_w/S_w = 100 \text{ cm}/3 \text{ cm}^2 = 25 \text{ cm}^{-1}$

=> **Voltage between windings** ($V = I \times R_w$ where $R_w = \kappa \times L_w/S_w$)

$V = 2000 \text{ [A]} \times 1.7E-6 \text{ [Ohm·cm]} \times 25 \text{ [cm}^{-1}] = 2.E-6 \times 5.E+4 \text{ [Ohm·A]}$

$V = 0.1 \text{ V.}$

From **Top Plot** ⁽¹⁾ we see **drift velocity** as $v = v(E/P)$ where

E - electric field, P =gas pressure.

In our case $E=0.1 \text{ [V cm}^{-1}]$; $P \sim 1000 \text{ [mmHg]}$ =>

$E/P = 1.E-4 \text{ [V cm}^{-1}/\text{mmHg]}$

From Top Plot we read $v(0.1) = 2.E+6 \text{ [cm/s]}$ and linear interpolation yields:

$v(1.E-4) = 2.E+3 \text{ [cm/s]}$.

From Bottom Plot for air we find $v(1.E-4) = 5.E+1 \text{ cm/s}$.

- (1) F. Sauli, "PRINCIPLES OF OPERATION OF MULTIWIRED PROPORTIONAL AND DRIFT CHAMBERS",

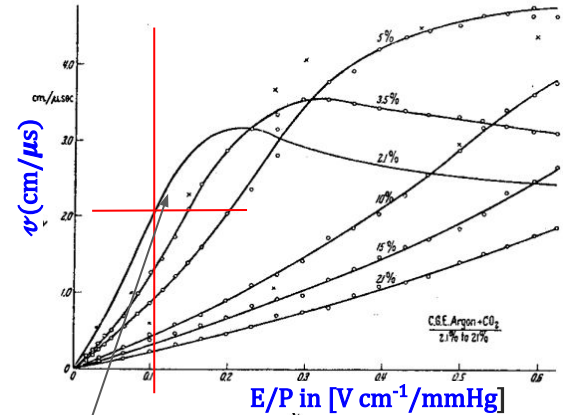


Fig. 29 Drift velocity of electrons in several argon-carbon dioxide mixtures⁽¹²⁾

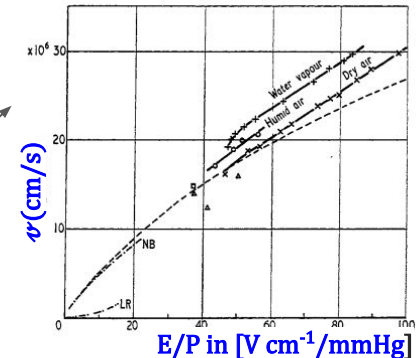


Figure 5. Electron drift velocity in dry air, humid air and water vapour as a function of reduced electrical field. Pressure readings reduced to temperature of 20 °C; humid air, $p_w/p = 16\%$. Broken line, Townsend and Tizard 1913; Δ , Raether; \square , Rieman 1944; NB, Nielsen and Bradbury 1937; LR, Lowe and Rees 1963.

2. What is leakage current between wires .

Current density between windings:

$$dI/ds \text{ [A/cm}^2\text{]} = n \text{ [e/cm}^3\text{]} \times v \text{ [cm/s]} \times 1.6\text{E-19 [C/e]} \propto v (\alpha^{-1} e_A)^{1/2}$$

Where $n=6.\text{E}+11 \text{ [e/cm}^3\text{]}$.

$v=2.\text{E}+3 \text{ [cm/s]}$.

For the current density we find :

$$\begin{aligned} dI/ds \text{ [A/cm}^2\text{]} &= 6.\text{E}+11[\text{e/cm}^3] \times 2.\text{E}+3 \text{ [cm/s]} \times 1.6\text{E-19 [C/e]} = 12 \times 1.6 \text{ E}(+11+3-19) = \\ &= 20.\text{E-5 [A/cm}^2\text{]}. \end{aligned}$$

Wire area $S=2 \text{ cm} \times 100 \text{ cm} = 2.\text{E}+2 \text{ cm}^2$, and the maximum possible current yields:

$$I \text{ [A]} = 20.\text{E-5 [A/cm}^2\text{]} \times 2.\text{E}+2 \text{ [cm}^2\text{]} = 40.\text{E-3 [A]} = 40 \text{ [mA]}. \text{ Compare to 2 kA !}$$

The voltage between entry lead of coil and ground will be 1 V!

Hence leak current form the first winding may be $I = 400 \text{ mA}$.

- Leakage is of $2.\text{E-5}$ of the wire current. It does not affects the coil performance.
- For Helium the leakage is ~ 10 times lower - due to the gas specific factor $v (\alpha^{-1} e_{\text{He}})^{1/2}$.

